Technical Memorandum

Wakulla Spring MFL: Hydrodynamic Model for MFL Evaluation of the Estuarine River

Prepared for: Northwest Florida Water Management District 81 Water Management Drive Havana, FL 32333-4712

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1 Introduction and Objectives

The Northwest Florida Water Management District (NWFWMD or District) is developing minimum flows and levels (MFLs) for Wakulla Spring and Sally Ward Spring in accordance with Section 373.042(1), Florida Statutes. The MFLs will address protection of water resources and ecology that may be affected by reduced spring flows due to future consumptive withdrawals. The MFL technical assessment for Wakulla Spring and Sally Ward Spring will quantify the limit of reductions in spring discharge commensurate with prevention of significant harm to the water resources or the ecology of the area, including those in the downstream freshwater and estuarine reaches of the Wakulla and St. Marks rivers.

Modeling tools have been previously developed to evaluate and predict the effects of spring flow reduction scenarios on selected water resource values (WRVs). These models include a mechanistic model for simulation of the hydrodynamic responses (salinity, temperature, water velocities, water surface elevation) within the combined St. Marks and Wakulla river systems to aid in determination of the St. Marks River and Wakulla River MFLs. This model was developed, calibrated, and used to evaluate flow reductions in the St. Marks River as part of the effort to establish the MFL for the St. Marks River Rise (NWFWMD, 2019).

The following sections of this document provide the results of a model review concerning the appropriateness of the existing hydrodynamic model construct for use in this effort, describes the selection of the baseline flow period for flow reduction scenario evaluation including the data used for model input, describes the WRVs of concern for the estuarine Wakulla River, and presents the results of the flow reduction scenarios evaluated with graphical and tabular presentation of comparison of the scenario results to those of the baseline condition.

2 Review of the Existing Hydrodynamic Model

An EFDC hydrodynamic model was previously developed (Janicki Environmental, 2018a) as part of the effort to establish the MFL for the St. Marks River Rise (NWFWMD, 2019). Prior to utilizing the existing model to evaluate effects of potential flow reductions in the estuarine portion of the Wakulla River, a review of the model was completed. This was necessary as the model was developed prior to the impacts on river physiography resulting from Hurricane Michael, which directly impacted the immediate area in October, 2018.

2.1 Model Development and Calibration

The model domain extends from approximately 2 miles (3 km) offshore of the mouth of the St. Marks River upstream to the US 98 bridge crossings on the St. Marks and the Wakulla. The District contracted bathymetric data collection from the mouth of the river upstream past the US 98 crossings (Wantman Group, Inc., 2016), and the bathymetry offshore of the mouth was developed using data obtained from the Florida Shelf Habitat (FLaSH) mapping study (Robbins et al., 2007). These data sources were used to develop the model grid bathymetry as described in Janicki Environmental (2018a) (Figures 1-3).

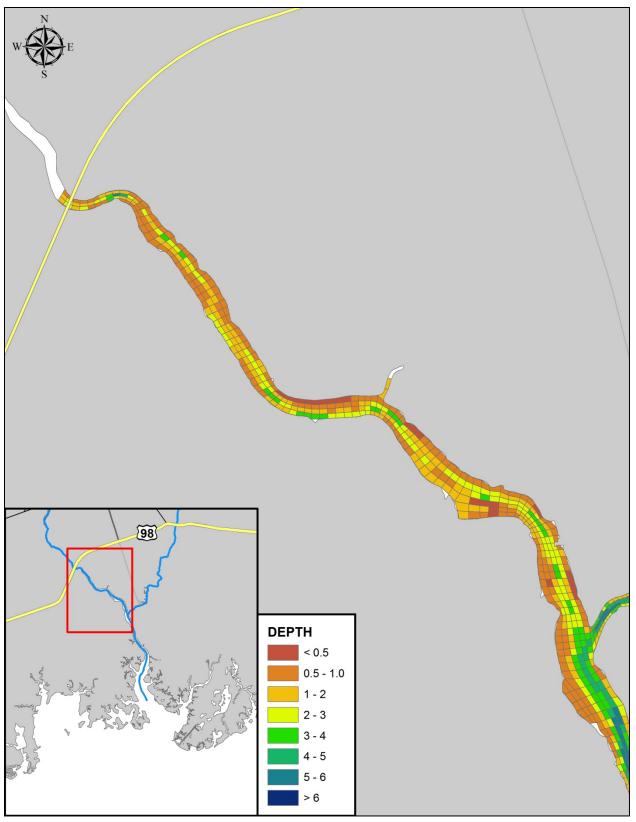


Figure 1. Model grid and bathymetry for the Wakulla River portion of the model domain. Vertical reference is NAVD88, vertical (depth) units are meters.

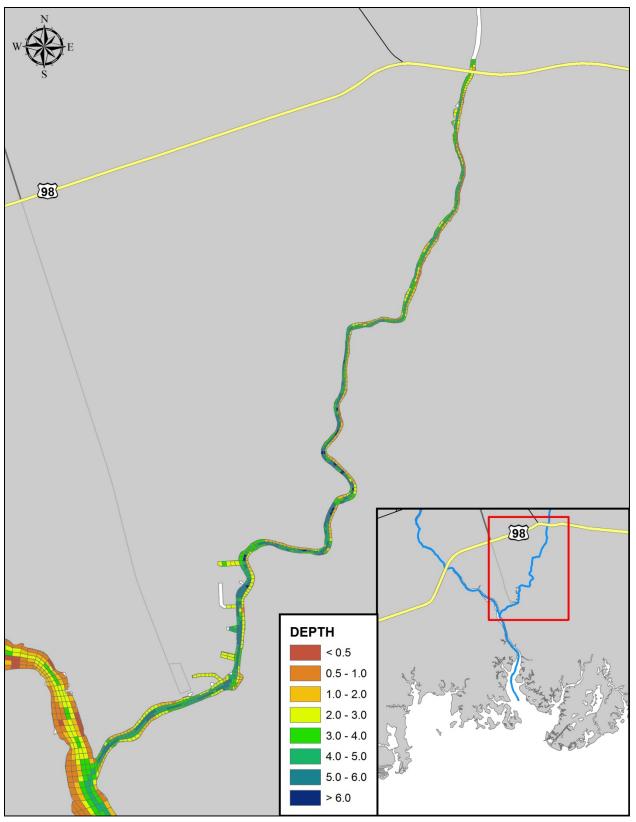


Figure 2. Model grid and bathymetry for the St. Marks River upstream of the confluence within the model domain. Vertical reference is NAVD88, vertical (depth) units are meters.

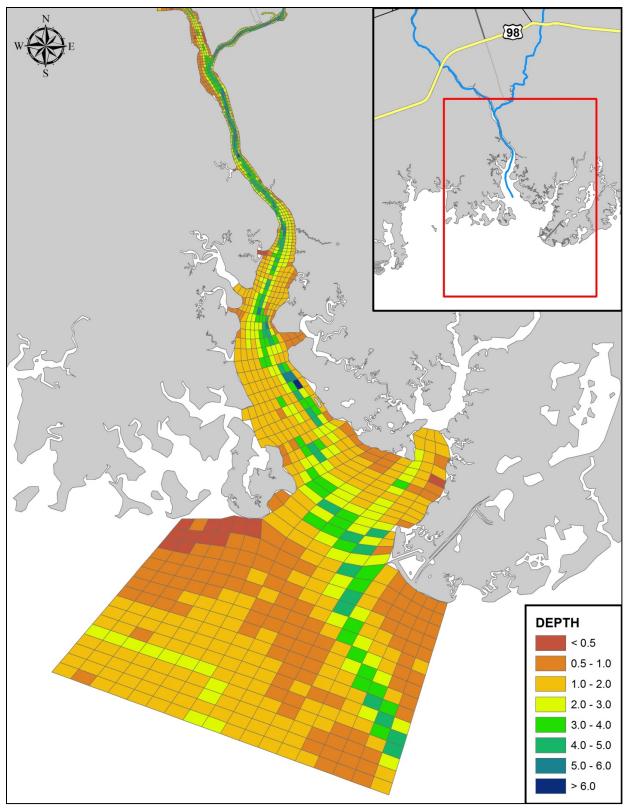


Figure 3. Model grid and bathymetry for the St. Marks River from the confluence downstream to the offshore boundary of the model domain. Vertical reference is NAVD88, vertical (depth) units are meters.

The hydrodynamic model was calibrated for the period May 11 - July 19, 2017; for a full description of the calibration see Janicki Environmental (2018a). Model inputs include the following, with the locations of the associated sites provided in Figure 4:

- Meteorological data from the National Weather Service Tallahassee Regional Airport site (air temperature, atmospheric pressure, relative humidity, rainfall, cloud cover), along with daily evapotranspiration and hourly solar radiation data from the FAWN IFAS site at Monticello, FL;
- Wind speed and direction data from the University of South Florida COMPS Shell Point site;
- Offshore surface water elevation boundary condition derived using measured data at continuous recorder HD-5 at the mouth of the river;
- Offshore boundary conditions for salinity and water temperature derived using measured data at HD-5;
- Upstream boundary conditions for salinity and water temperature as measured at continuous recorders HD-1 and HD-2;
- Initial conditions for salinity and water temperature derived from the five continuous recorders (HD-1 through HD-5); and
- Freshwater inflows from the USGS gages St. Marks near Newport (02326900) and Wakulla near Crawfordville (02327022), with ungaged inflows estimated as part of the HEC-RAS work completed for the St. Marks River Rise MFL development.

Model calibration was accomplished by comparing model output to observed data. This was completed for water surface elevation data collected at all five continuous recorders (HD-1 through HD-5, Figure 4), and for surface and bottom salinity using data collected at HD-5, HD-4, and HD-3. Additionally, longitudinal salinity profile data were collected in both the St. Marks River and Wakulla River (Figure 5), with these data compared to model output. A further test of the model was completed by comparing modeled cross-river water flux to data collected for this purpose.

The results of the calibration effort showed that the hydrodynamic model was appropriately calibrated to evaluate the responses in the river to potential flow reductions. The model was then used to evaluate expected effects of potential spring flow reductions from the St. Marks River Rise in aid of MFL development (Janicki Environmental, 2018b).

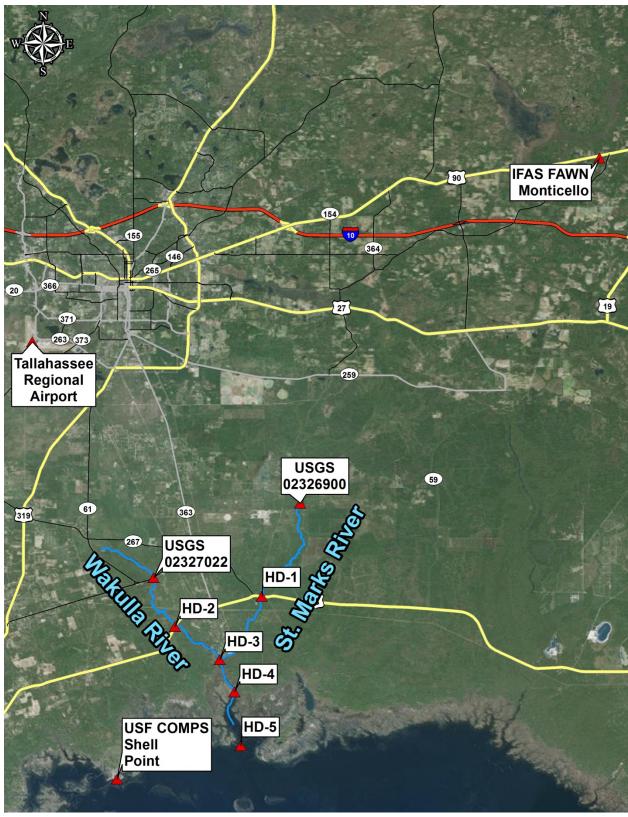


Figure 4. Locations of data collection sites for continuous recorders (HD-1 through HD-5), USGS flow gages, USF COMPS Shell Point winds, Tallahassee Regional Airport meteorology (including rainfall), and IFAS FAWN Monticello.

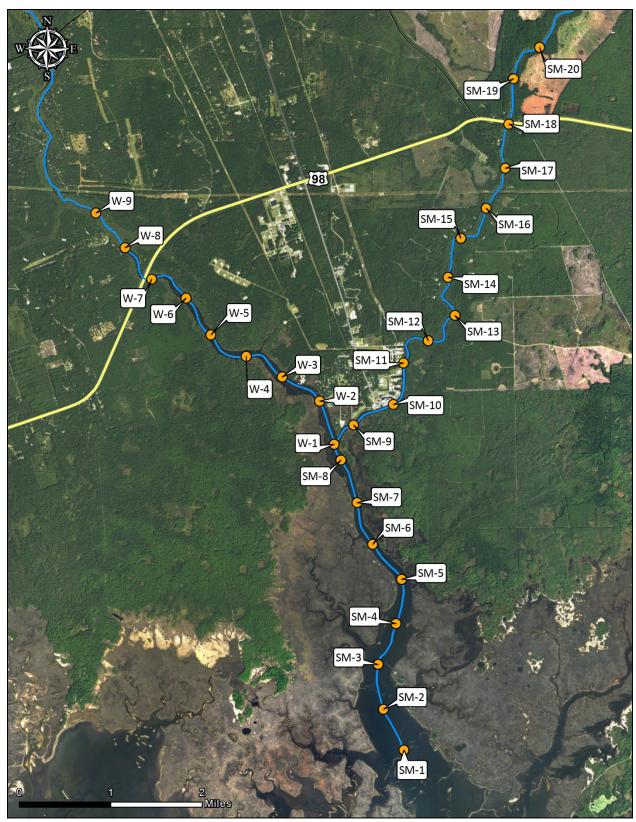


Figure 5. Locations of vertical profile sampling sites in St. Marks River and Wakulla River.

2.2 Review for Appropriateness Post-Hurricane Michael

Hurricane Michael impacted the St. Marks/Wakulla region in October 2018, after the initial bathymetry data collection that was used for developing the model grid bathymetry. Post-Michael, the District obtained updated bathymetric data for the Wakulla River after observing some scouring of the river bed downstream of the spring. However, these effects were limited to the region upstream of the US 98 bridge, the upstream-most extent of the model domain in the Wakulla River. The updated bathymetry data were collected primarily upstream of the US 98 bridge, with updated data collected at only a few locations along the banks downstream of the bridge (Figure 6). Evaluation of these data with respect to the existing bathymetry for the model grids indicated that there was no need to revise the model bathymetry in the Wakulla River portion of the model domain.

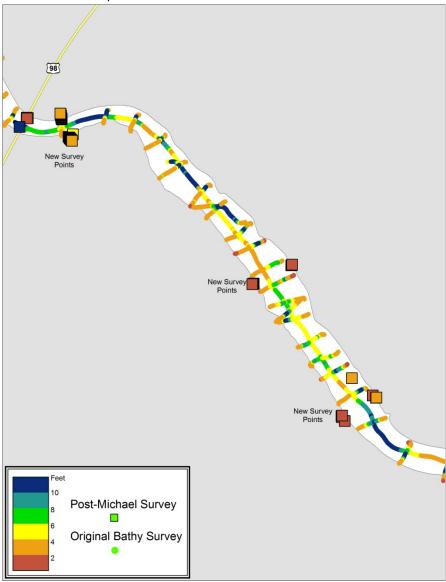


Figure 6. Locations of new transect data collection sites for elevation (squares marked as "New Survey Points") with original bathymetric data in the Wakulla River below the US 98 crossing.

3 Determination of Baseline Period

The long-term record for Wakulla river flows at the USGS gage 02327022, Wakulla River near Crawfordville (at Shadeville Rd), begins in 2004. Using this record for the entire period of 2004-2019 provides a flow distribution to guide the selection of a shorter time period, one amenable to modeling evaluation. Examination of consecutive 2- and 3-yr periods resulted in selection of the flow record for January 1, 2008 - October 4, 2010, as most representative of the long-term flow distribution (Figure 7). The flow distribution statistics for the period of record and the selected baseline period are provided in Table 1.

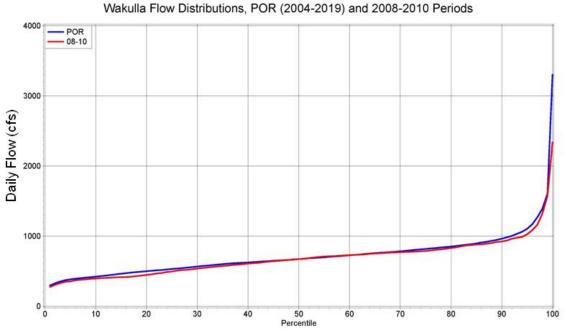


Figure 7. Comparison of flow distributions at USGS gage 02327022, for period of record (2004-2019) and 2008-2010.

Table 1. Distribution of flows during period of record (2004-2019) and selected baseline period.								
Flow Percentiles								
	(cfs)	Flow (cfs)						
5 th	383.9	354.5						
10 th	421.5	395.7						
25 th	531.0	495.7						
50 th	672.6	673.0						
75 th	817.7	788.5						
90 th	963.7	922.8						
95 th	1103.5	1026.5						
Mean	700.5	676.2						

The input data for the Baseline Scenario were compiled and prepared for input to the EFDC hydrodynamic model, for the period December 1, 2007 - October 4, 2010, with the December 2007 data

providing for a 1-month spinup of the model prior to the baseline period. These data included the following:

- Meteorological and Wind Data:
 - Air Temperature: Tallahassee Airport, NWS (hourly)
 - Atmospheric Pressure: Tallahassee Airport, NWS (hourly)
 - Relative Humidity: Tallahassee Airport, NWS (hourly)
 - Rainfall: Tallahassee Airport, NWS (hourly)
 - Cloud Cover: Tallahassee Airport, NWS (hourly)
 - Evapotranspiration: Monticello, UF IFAS FAWN (daily)
 - Solar Radiation: Monticello, UF IFAS FAWN (hourly)
 - Wind Speed and Direction: Shell Point, USF COMPS (6-minute), with missing data filled from USF COMPS Keaton Beach site
- Water Surface Elevation Offshore Boundary Condition:
 - Air Temperature: Tallahassee Airport, NWS (hourly)
- Salinity and Temperature Offshore Boundary Conditions:
 - Gulf Coast Shelf Model (GCSM) output at the offshore river model limit, as used in the St. Marks MFL flow reduction scenarios evaluation (Janicki Environmental, 2018b). The GCSM output used was for June 1997 May 1999, with mean values taken by day and month to develop the offshore records for salinity and temperatures.
- Freshwater Inflows:
 - Wakulla River: gaged flows at USGS 02327022 (daily)
 - St. Marks River: gaged flows at USGS 02326900 (daily) adjusted to account for the St. Marks
 River Rise MFL, and adjusted for downstream ungaged flows between the gage and the
 upstream model extent as estimated as part of the HEC-RAS work completed for the St.
 Marks River Rise MFL development.

Time series plots of hourly meteorological data are provided in Figures 8-14, with the NWS site at Tallahassee Regional Airport providing relative humidity, atmospheric pressure, air temperature, cloud cover, and rainfall. Hourly solar radiation data were obtained for the IFAS FAWM Monticello site, along with daily evapotranspiration data.

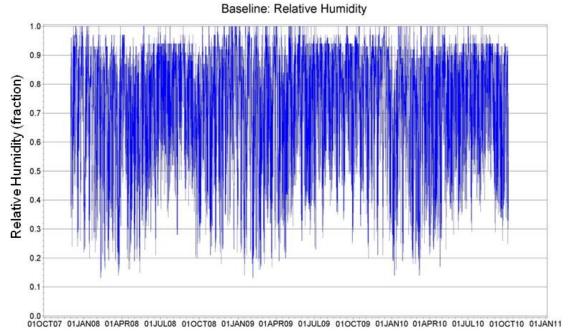


Figure 8. Hourly relative humidity from Tallahassee NWS site, December 1, 2007 to October 4, 2010.

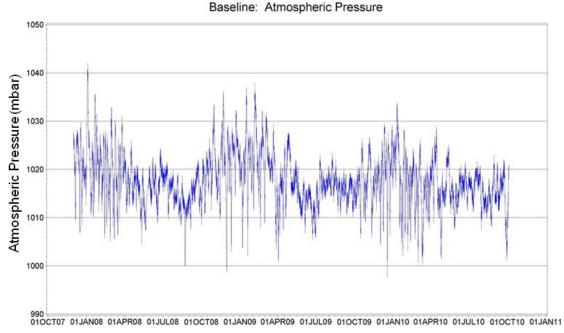


Figure 9. Hourly atmospheric pressure from Tallahassee NWS site, December 1, 2007 to October 4, 2010.

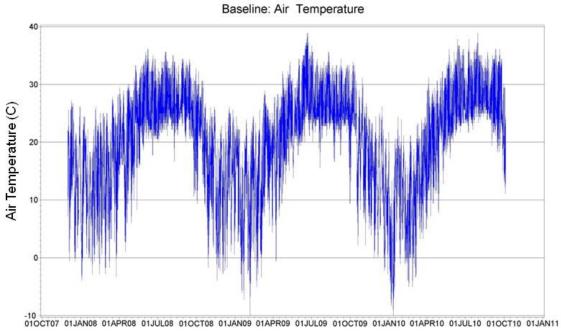


Figure 10. Hourly air temperature from Tallahassee NWS site, December 1, 2007 to October 4, 2010.

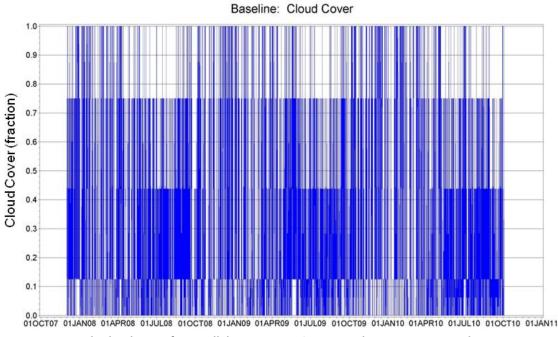


Figure 11. Hourly cloud cover from Tallahassee NWS site, December 1, 2007 to October 4, 2010.

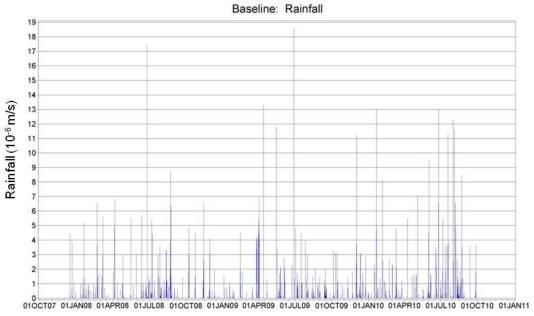


Figure 12. Hourly rainfall from Tallahassee NWS site, December 1, 2007 to October 4, 2010.

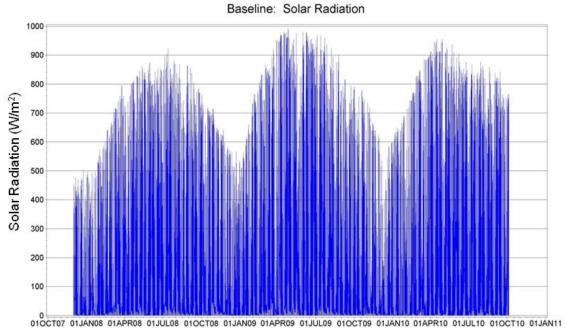


Figure 13. Hourly solar radiation from Monticello IFAS FAWN site, December 1, 2007 to October 4, 2010.

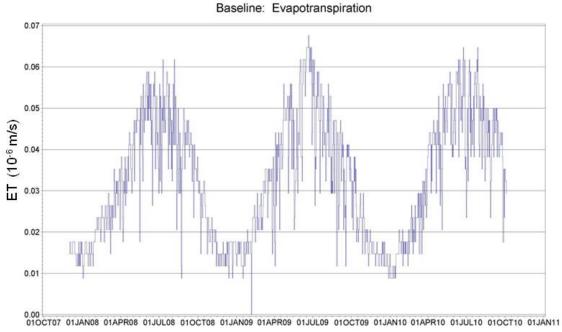


Figure 14. Daily evapotranspiration from Monticello IFAS FAWN site, December 1, 2007 to October 4, 2010.

Wind speed and wind direction data for the baseline period were obtained at 6-minute frequency from the USF COMPS Shell Point site on the Gulf Coast, with time series plots of wind speed and direction provided in Figures 15 and 16, respectively.

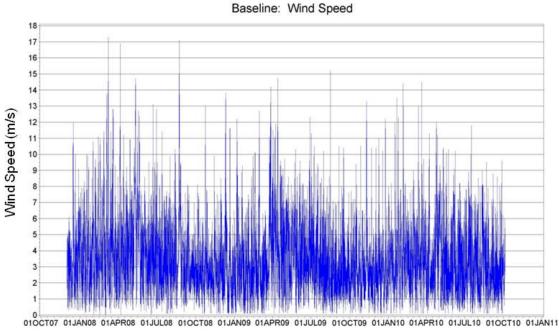


Figure 15. 6-minute frequency wind speed from Shell Point USF COMPS site, December 1, 2007 to October 4, 2010.

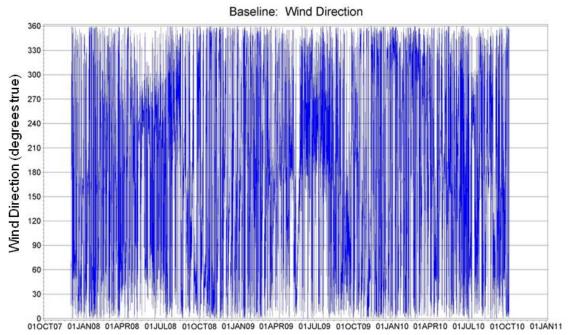


Figure 16. 6-minute frequency wind direction from Shell Point USF COMPS site, December 1, 2007 to October 4, 2010.

Predicted water surface elevations at the St. Marks Lighthouse on Apalachee Bay were obtained from NOAA/NOS/CO-OPS daily tide prediction website at 6-minute intervals, and used to set the offshore water surface elevation boundary condition. The time series for December 1, 2007 - October 4, 2010 is provided in Figure 17.

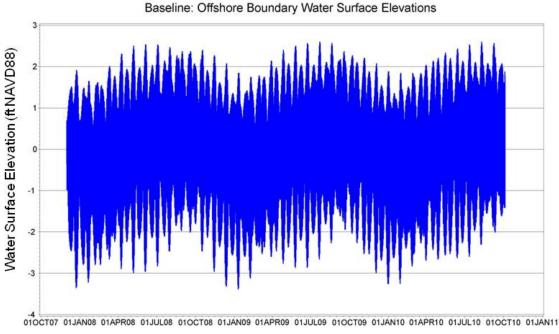


Figure 17. Water surface elevations at St. Marks Lighthouse on Apalachee Bay, from NOAA/NOS/CO-OPS, for December 1, 2007 to October 4, 2010, used for downstream boundary condition.

For the offshore boundary conditions for salinity and temperature, no data for the model period were available. Since the comparison of flow reduction scenarios to baseline conditions requires that the offshore boundaries be the same for each model implementation, it was only necessary that the offshore boundaries for salinity and temperature be reasonable and unmodified between scenarios. To this end, the offshore boundary conditions as utilized for the St. Marks MFL scenario evaluation (Janicki Environmental, 2018b) were used to develop salinity and temperature time series records for the baseline Wakulla evaluation. Hourly records as output from the GCSM for the offshore boundary during June 1997 - May 1999 were selected as being reasonable, as these were also used for the St. Marks evaluation. Mean values by calendar day and hour were developed, so that the boundary conditions were the same for a given calendar day and hour of each year of the baseline model period. These time series of salinity and temperature are provided in Figures 18 and 19, respectively.

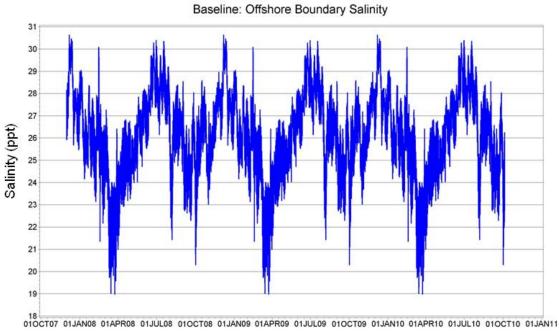


Figure 18. Salinity used for downstream boundary condition derived from offshore GCSM output.

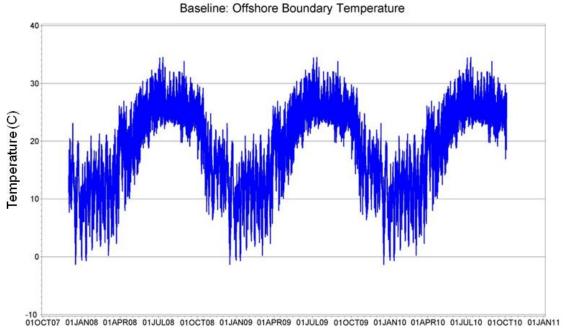


Figure 19. Water temperature used for downstream boundary condition derived from offshore GCSM output.

Freshwater inflows are from the USGS gages St. Marks near Newport (02326900) and Wakulla near Crawfordville (02327022), with ungaged inflows to the St. Marks River between the gage and the upstream extent of the model domain estimated as part of the HEC-RAS work completed for the St. Marks River Rise MFL development. In addition, the adopted St. Marks River Rise minimum flow is accounted for by a 7.3% reduction in the spring flow contribution to the gaged flow at 02326900. The freshwater inflows to the model are provided in Figures 20 and 21, for the Wakulla River and St. Marks River, respectively.

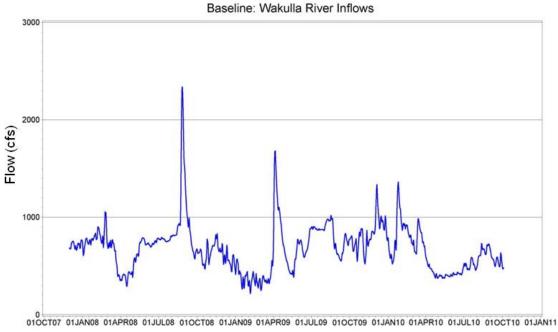


Figure 20. Freshwater flows to upstream baseline model in Wakulla River.

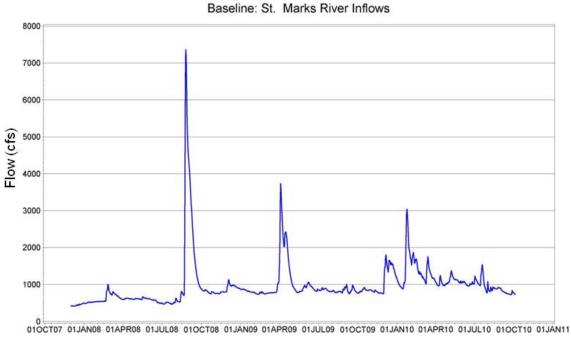


Figure 21. Freshwater flows to upstream baseline model in St. Marks River.

4 Definition of Water Resource Values (WRVs)

Multiple metrics were evaluated for Estuarine Resources, including the volume, bottom surface area, and shoreline length for a set of oligohaline (i.e. low salinity) zones, including ≤ 0.5 ppt, ≤ 1 ppt, ≤ 2 ppt, ≤ 3

ppt, and ≤4 ppt. This set of metrics is the same as that utilized for the Estuarine Resources evaluation of the St. Marks River Rise MFL (NWFWMD, 2019). Volume was considered as a metric to protect fish species habitat, bottom surface area to protect benthic species habitat, and shoreline length for the protection of shoreline floodplain vegetation communities.

5 Evaluation of Flow Reduction Scenarios and Sea Level Rise Scenario

Two flow reduction scenarios were evaluated for the potential impacts on the Estuarine Resource WRVs for the Wakulla and Sally Ward Spring evaluation. In the first, a flow reduction of 30% was applied at the USGS Wakulla River gage (02327022). The second flow reduction evaluated was 36%, also applied at the Wakulla River gage. Both flow reductions were directly applied to the input flows to the upstream end of the model domain for the Wakulla River. The evaluation of WRVs was made for the estuarine portion of the Wakulla River, between the US 98 crossing of the Wakulla River and the downstream conjunction with the St. Marks River.

For this WRV metric comparison, two different analyses were completed. First, the average daily volumes, bottom areas, and shoreline lengths of each salinity envelope (≤ 0.5 ppt, ≤ 1 ppt, ≤ 2 ppt, ≤ 3 ppt, and ≤ 4 ppt) were calculated over the 01/01/08-10/03/10 period for each scenario (the last day of the model period, 10/04/10, was not completed for the full 24-hour period due to an incomplete wind data input file, which was short by 4 fours due to correction of the timestamp from UTC to EST). Then, both the median and mean metric values for each salinity envelope over the full period were calculated.

Table 2 below provides these results comparing the baseline scenario and the 30% Wakulla River flow reduction run for the Wakulla River portion of the model domain (that area from the confluence upstream to the US98 bridge crossing of the Wakulla River), using the median of the daily average values for comparison. Table 3 similarly shows comparison results, based on the average (not the median) of the daily average values. As shown in both Tables 2 and 3, the reduction in WRV metrics within the estuarine Wakulla River (confluence upstream to the US98 Bridge) for a 30% river flow reduction never reached 15%, indicating that estuarine resource metrics are relatively insensitive to reductions in flow at this level from Wakulla Spring. This is due to the mean flow of 676 cfs for the baseline period, which even reduced by 30% is still more than 470 cfs mean daily flow. The average river volume for the baseline flow record between the confluence and the US 98 bridge is 1.02 million m³. The average flow rate of 676 cfs for the baseline is equivalent to 1.65 million m³. The average daily flow through the river between the confluence and the US 98 bridge is thus 1.6 times the average river volume, so that most of the river in this region is relatively fresh (<4 ppt) (Table 2). The flow reduction of 30% still results in the total daily flow volume being greater than the river volume in this region (1.1 times), so that even at this flow reduction level most of the river volume here is <4 ppt.

An additional scenario with a 36% flow reduction to the estuarine Wakulla River was implemented to determine if this great a reduction would result in exceedence of the 15% habitat reduction level for any of the metrics. Tables 4 and 5 below contain the results of this effort, with Table 4 providing a

comparison of the medians of the daily average values, and Table 5 the average of the daily average values. Based on this scenario, a reduction of >15% was found for the ≤ 1 ppt extent of bottom area (Table 3), as well as reductions >15% for the ≤ 0.5 ppt metrics.

Time series plots of the resultant habitat metrics from the baseline and two flow reduction scenarios are provided in Appendix 1, along with those of the Sea Level Rise scenario (described below).

Table 2. Comparison of WRV metrics for median volume, bottom area, and shoreline length in estuarine							
Wakulla River for baseline (Base) and flow reduction (30%) scenarios.							
Scenario	Volume ≤ 0.5 ppt (m³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction	
Base	852,096	146	529,980	13.6	9,675	0.0	
30% Reduction	727,709	14.6	458,054	13.0	8,870	8.3	
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 1 ppt (m³)	Reduction	1 ppt (m²)	Reduction	1 ppt (m)	Reduction	
Base	908,972	11.4	571,531	12.6	9,863	2.9	
30% Reduction	805,273	11.4	499,659	12.0	9,572	2.9	
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 2 ppt (m³)	Reduction	2 ppt (m²)	Reduction	2 ppt (m)	Reduction	
Base	962,040	6.5	605,710	7.2	9,863	0.0	
30% Reduction	899,514	6.5	561,270	7.3	9,863	0.0	
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 3 ppt (m³)	Reduction	3 ppt (m ²)	Reduction	3 ppt (m)	Reduction	
Base	985,263	2.0	637,117	6.3	9,863	0.0	
30% Reduction	947,326	3.9	597,919	6.2	9,863	0.0	
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 4 ppt (m³)	Reduction	4 ppt (m²)	Reduction	4 ppt (m)	Reduction	
Base	1,000,640	2.0	646,681	4.1	9,863	0.0	
30% Reduction	970,173	3.0	619,954	4.1	9,863	0.0	

Table 3. Comparison of WRV metrics for average volume, bottom area, and shoreline length in estuarine Wakulla River for baseline (Base) and flow reduction (30%) scenarios.							
Scenario	Volume ≤ 0.5 ppt (m³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction	
Base	848,704	12.4	537,577	12.2	9,395	7.5	
30% Reduction	743,270	12.4	472,257	12.2	8,690	7.5	
Scenario	Volume ≤ 1 ppt (m³)	Percent Reduction	Bottom Area ≤ 1 ppt (m²)	Percent Reduction	Shoreline ≤ 1 ppt (m)	Percent Reduction	
Base	900,463	10.2	568,113	10.7	9,730	4.1	
30% Reduction	808,393	10.2	507,388	10.7	9,336	4.1	
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 2 ppt (m³)	Reduction	2 ppt (m²)	Reduction	2 ppt (m)	Reduction	
Base	953,935	6.7	604,736	7.4	9,849	0.7	
30% Reduction	889,837	0.7	449,939	77	9,785	0.7	
Scenario	Volume ≤ 3 ppt (m³)	Percent Reduction	Bottom Area ≤ 3 ppt (m²)	Percent Reduction	Shoreline ≤ 3 ppt (m)	Percent Reduction	
Base	982,222	4.0	627,712	F 3	9,860	0.1	
30% Reduction	935,537	4.8	595,172	5.2	9,849		
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent	
	≤ 4 ppt (m³)	Reduction	4 ppt (m²)	Reduction	4 ppt (m)	Reduction	
Base	998,509	3.4	642,314	3.8	9,862	0.0	
30% Reduction	964,274	J.4 	617,991	3.0	9,860	0.0	
Table 4. Comparison of WRV metrics for median volume, bottom area, and shoreline length in estuarine							

Wakulla River for baseline (Base) and flow reduction (36%) scenarios.							
Scenario	Volume ≤ 0.5 ppt (m³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction	
Base	852,096	18.8	529,980	20.7	9,675	11.0	
36% Reduction	692,080		420,172		8,615		
Scenario	Volume ≤ 1 ppt (m³)	Percent Reduction	Bottom Area ≤ 1 ppt (m²)	Percent Reduction	Shoreline ≤ 1 ppt (m)	Percent Reduction	
Base 36% Reduction	908,972 774,260	14.8	571,531 484,004	15.3	9,863 9,548	3.2	
Scenario	Volume ≤ 2 ppt (m³)	Percent Reduction	Bottom Area ≤ 2 ppt (m²)	Percent Reduction	Shoreline ≤ 2 ppt (m)	Percent Reduction	
Base 36% Reduction	962,040 877,016	8.8	605,710 543,769	10.2	9,863 9,863	0.0	
Scenario	Volume ≤ 3 ppt (m³)	Percent Reduction	Bottom Area ≤ 3 ppt (m²)	Percent Reduction	Shoreline ≤ 3 ppt (m)	Percent Reduction	
Base 36% Reduction	985,263 932,866	5.3	637,117 589,625	7.5	9,863 9,863	0.0	
Scenario	Volume ≤ 4 ppt (m³)	Percent Reduction	Bottom Area ≤ 4 ppt (m²)	Percent Reduction	Shoreline ≤ 4 ppt (m)	Percent Reduction	
Base 36% Reduction	1,000,640 959,514	4.1	646,681 607,284	6.1	9,863 9,863	0.0	

Table 5. Comparison of WRV metrics for average volume, bottom area, and shoreline length in estuarine Wakulla River for baseline (Base) and flow reduction (36%) scenarios.							
Scenario	Volume ≤ 0.5 ppt (m³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction	
Base	848,704	15.9	537,577	16.1	9,395	9.1	
36% Reduction	713,771	13.9	450,964	10.1	8,534	9.1	
Scenario	Volume ≤ 1 ppt (m³)	Percent Reduction	Bottom Area ≤ 1 ppt (m²)	Percent Reduction	Shoreline ≤	Percent Reduction	
Base		Reduction		Reduction	1 ppt (m)	Reduction	
36% Reduction	900,463 780,139	13.4	568,113 486,067	14.4	9,730 9,262	4.8	
Scenario	Volume ≤ 2 ppt (m³)	Percent Reduction	Bottom Area ≤ 2 ppt (m²)	Percent Reduction	Shoreline ≤ 2 ppt (m)	Percent Reduction	
Base 36% Reduction	953,935 867,984	9.0	604,736 541,153	10.5	9,849 9,801	0.5	
Scenario	Volume ≤ 3 ppt (m³)	Percent Reduction	Bottom Area ≤ 3 ppt (m²)	Percent Reduction	Shoreline ≤ 3 ppt (m)	Percent Reduction	
Base 36% Reduction	982,222 918,572	6.5	627,712 582,440	7.2	9,860 9,861	0.0	
Scenario	Volume ≤ 4 ppt (m³)	Percent Reduction	Bottom Area ≤ 4 ppt (m²)	Percent Reduction	Shoreline ≤ 4 ppt (m)	Percent Reduction	
Base 36% Reduction	998,509 950,684	4.8	642,314 608,762	5.2	9,862 9,863	0.0	

In addition to the flow reduction scenario, a Sea Level Rise scenario was implemented, accounting for a potential increase in sea level of 1.87 inches. This value represents the estimated increase in sea level

using the average (2.38 mm/yr) observed long-term sea level rise rates provided by NOAA for Apalachicola (2.56 mm/yr) and Cedar Key, Florida (2.19 mm/yr) (NOAA 2020). This increase was applied over the full period of the comparison run, 1/1/08-10/04/10. The resultant changes in WRV metrics are provided in Tables 6 and 7 below, for the medians of the daily average values (Table 6) and the average of the daily average values (Table 7). Time series plots of the habitat metric values are provided in Appendix 1. Results indicate that a sea level rise of 1.87 inches is likely to have an impact of some estuarine resource metrics. The effects of sea level rise in combination with Wakulla River flow reductions was not estimated.

Table 6. Comparison of WRV metrics for median volume, bottom area, and shoreline length in estuarine								
Wakulla River for baseline (Base) and sea level rise (SLR) scenarios.								
Scenario	Volume ≤ 0.5 ppt (m ³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m ²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction		
Base	852,096	2.2	529,980	4.9	9,675	0.6		
SLR	832,500	2.3	503,961	4.9	9,623	0.6		
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent		
	≤ 1 ppt (m³)	Reduction	1 ppt (m²)	Reduction	1 ppt (m)	Reduction		
Base	908,972	0.6	571,531	6.2	9,863	0.0		
SLR	903,429	0.0	536,312	0.2	9,863			
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent		
	≤ 2 ppt (m³)	Reduction	2 ppt (m²)	Reduction	2 ppt (m)	Reduction		
Base	962,040	0.0	605,710	1.6	9,863	0.0		
SLR	969,487	-0.8	596,337	1.6	9,863	0.0		
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent		
	≤ 3 ppt (m³)	Reduction	3 ppt (m ²)	Reduction	3 ppt (m)	Reduction		
Base	985,263	4.5	637,117	2.5	9,863	0.0		
SLR	999,519	-1.5	615,132	3.5	9,863	0.0		
Scenario	Volume	Percent	Bottom Area ≤	Percent	Shoreline ≤	Percent		
	≤ 4 ppt (m³)	Reduction	4 ppt (m²)	Reduction	4 ppt (m)	Reduction		
Base	1,000,640	1.6	646,681	1.2	9,863	0.0		
SLR	1,016,341	-1.6	639,258	1.2	9,863	0.0		

Table 7. Comparison of WRV metrics for average volume, bottom area, and shoreline length in estuarine Wakulla River for baseline (Base) and sea level rise (SLR) scenarios.							
Scenario	Volume ≤ 0.5 ppt (m³)	Percent Reduction	Bottom Area ≤ 0.5 ppt (m²)	Percent Reduction	Shoreline ≤ 0.5 ppt (m)	Percent Reduction	
Base	848,704	1 1	537,577	F 2	9,395	0.6	
SLR	839,144	1.1	509,232	5.3	9,337	0.6	
Scenario	Volume ≤ 1 ppt (m³)	Percent Reduction	Bottom Area ≤ 1 ppt (m²)	Percent Reduction	Shoreline ≤ 1 ppt (m)	Percent Reduction	
Base SLR	900,463 896,374	0.5	568,113 542,442	4.5	9,730 9,745	-0.2	
Scenario	Volume ≤ 2 ppt (m³)	Percent Reduction	Bottom Area ≤ 2 ppt (m²)	Percent Reduction	Shoreline ≤ 2 ppt (m)	Percent Reduction	
Base SLR	953,935 958,580	-0.5	604,736 587,014	2.9	9,849 9,860	-0.1	
Scenario	Volume ≤ 3 ppt (m³)	Percent Reduction	Bottom Area ≤ 3 ppt (m²)	Percent Reduction	Shoreline ≤ 3 ppt (m)	Percent Reduction	
Base SLR	982,222 992,876	-1.1	627,712 614,646	2.1	9,860 9,863	0.0	
Scenario	Volume ≤ 4 ppt (m³)	Percent Reduction	Bottom Area ≤ 4 ppt (m²)	Percent Reduction	Shoreline ≤ 4 ppt (m)	Percent Reduction	
Base SLR	998,509 1,013,774	-1.5	642,314 631,561	1.7	9,862 9,863	0.0	

6 Conclusions

A baseline model scenario was developed and implemented for the period 1/01/08-10/04/10, when the Wakulla River flow distributions were very similar to those for the full period of record, from 2004-2019. Two flow reduction scenarios were implemented and evaluated along with a sea level rise scenario. It required a 36% flow reduction to reach a habitat metric reduction of 15% or greater in the estuarine Wakulla River, with a 30% flow reduction resulting in no habitat metrics reduced by 15% or more relative to the baseline conditions.

The results also indicated that changes in low-salinity habitat metrics within the estuarine Wakulla River are not linear with respect to flow reductions. Overall, salinity habitat metrics within the estuarine river are relatively insensitive to changes in flow from Wakulla Spring.

7 References

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